

# Exact numerical solution for a time-dependent fibre-bundle model with continuous damage

L Moral<sup>1</sup>, J B Gómez<sup>2</sup>, Y Moreno<sup>3</sup> and A F Pacheco<sup>4</sup>

<sup>1</sup> Departamento de Matemática Aplicada, Universidad de Zaragoza, 50009 Zaragoza, Spain

<sup>2</sup> Departamento de Ciencias de la Tierra, Universidad de Zaragoza, 50009 Zaragoza, Spain

<sup>3</sup> The Abdus Salam International Centre for Theoretical Physics, Condensed Matter Group, PO Box 586, Trieste, I-34014, Italy

<sup>4</sup> Departamento de Física Teórica, Universidad de Zaragoza, 50009 Zaragoza, Spain

Received 4 July 2001, in final form 11 September 2001

Published 16 November 2001

Online at [stacks.iop.org/JPhysA/34/9983](http://stacks.iop.org/JPhysA/34/9983)

## Abstract

A time-dependent global fibre-bundle model of fracture with continuous damage was recently formulated in terms of an autonomous differential system and numerically solved by applying a discrete probabilistic method. In this paper we provide a method to obtain the exact numerical solution for this problem. It is based on the introduction of successive integrating parameters which permits a robust inversion of the numerical integrations appearing in the problem.

PACS numbers: 46.50.+a, 02.60.-x, 62.20.Fe, 62.20.Mk

## 1. Introduction

Fracture in disordered media has for many years attracted much scientific and industrial interest [1–7]. An important class of models of material failure is the fibre-bundle models (FBMs) which have been extensively studied during the past decades [7–12]. These models consist of a set of parallel fibres having statistically distributed strengths. The sample is loaded parallel to the fibre direction, and a fibre fails if the load acting on it exceeds a strength threshold value. When a fibre fails, its load is transferred to other surviving fibres in the bundle according to a specific transfer rule. Among the possible options of load transfer, one simplification that makes the problem analytically tractable is the assumption of equal load sharing (ELS), or global load transfer, which means that after each fibre breaks, its stress is equally distributed among the intact fibres. Until very recently, the failure rule applied in standard FBM was discontinuous and irreversible, i.e., when the local load exceeds the failure threshold of a fibre, the fibre is removed from the calculation and is never restored. Recently, a novel continuous damage law was incorporated into these models [13, 14]. Thus, when the strength threshold of a fibre is exceeded, it yields, and the elastic modulus of the fibre is reduced by a factor  $a$  ( $0 < a < 1$ ). Multiple yields

of a given fibre are allowed, up to a maximum of  $n$  yielding events per fibre, where  $n$  is a small integer number which can be different for each fibre. This generalization of the standard FBM is suitable to describe a variety of elasto-plastic constitutive behaviours [15–17].

The standard FBMs simulate the failure of a system at the *microscopic* level. Each fibre breakage can be mapped onto a new microcrack (with a typical size of a few  $\mu\text{m}$ ), or onto the extension of a previous microcrack. On the other hand, the continuous damage FBMs simulate failure at a *mesoscopic* level. Now, each fibre in the model can be viewed as a small volume of the material. The term ‘small’ depends on the size of the heterogeneities, but can be of the order of one millimetre for rocks. In each of these representative elementary volumes (REVs) in which the total volume can be divided, there are many potential sites for crack nucleation and growth, and the addition of each new crack will change continuously the elastic properties of the REV until its final failure when the accumulated damage surpasses a threshold. This threshold is identified in our model with the parameter  $n$ . Another important parameter in the model, the stiffness reduction factor  $a$ , controls the amount of weakening that each yielding event introduces in an REV. The value  $a = 1$  means no weakening, so that the elastic modulus of the REV remains the same irrespective of the number of yieldings, a rather unphysical situation. At the other extreme, the value  $a = 0$  means complete weakening after the first yield event. Thus,  $0 < a < 1$  is the physically meaningful range for the stiffness reduction factor. In all the results given in the following sections, we have assumed that the initial elastic module of all the REVs is unity and that  $n$  is the same for all the fibres. The randomness is incorporated in the lifetimes of REVs not in the elastic moduli.

FBMs come in two settings, static and time-dependent or dynamic, and both of them have been applied to the standard and continuous damage settings [13, 14, 18, 19]. The static version of FBM simulates the failure of materials by quasistatic loading. Drawing an analogy with what is carried out in a deformation experiment in the laboratory: a static FBM simulates a uniaxial or triaxial, compressive or tensile, deformation test where the duration of the test is measured in seconds or minutes. In these models, the stress on each fibre is the independent variable and the strength of each element is the distributed random variable. On the other hand, the dynamic FBM simulates failure by creep rupture, static fatigue, or delayed rupture, i.e., a (usually) constant load is imposed on the system and the elements break because of fatigue after a period of time. The time elapsed until the system collapses is the lifetime of the bundle. Time acts as an independent variable and the initial lifetime of each element for a prescribed initial stress in the independent identically distributed random quantity. Again, we can draw a clear analogy with a particular type of deformation experiments in the laboratory, the so-called creep experiments, where a heterogeneous material (rock, concrete, composite, ceramic alloy) is subjected to a constant or cyclic load, breaking after a period of time. The duration of these tests depends on the load imposed on the material and, more exactly, on the load compared to the short-term strength of the material (i.e., the load that causes the ‘instantaneous’ failure of the same material in a fast uniaxial experiment). This load is usually expressed as a percentage of the short-term strength and the duration of the experiments is critically dependent on it. For rock, a sample will typically fail by creep after a few hours when subjected to a load 80% of the short-term strength, after a few weeks for a load 70% of the short-term strength and after a few months or even years for lower working loads. The mechanism behind creep failure is *subcritical crack growth*, i.e., the slow extension of microcracks with lengths smaller than the critical crack length for instantaneous failure. Subcritical crack growth is due to a variety of processes operating near crack tips, the most important of them being *stress corrosion*, a chemical interaction

between the crack tip and the environmental species, notably water, filling the microcracks that provoke the hydrolytic weakening of the atomic bonds of the material in the crack tip, where stress concentrations are highest. The crack propagation velocity is extremely sensitive to the applied load, suggesting exponential or power-law velocity functions with large coefficients or exponents.

Indeed, in the dynamic FBMs the most widely used breaking rate function is the power law [10–12], in which elements break at a rate proportional to a power of their stress  $\sigma^\rho$ , where the exponent  $\rho$  is an integer known as the stress corrosion exponent for obvious reasons. This type of breaking rate will be assumed here and  $\rho$  is another parameter of the model.

Our generalization of the dynamic global FBM [18] was restricted to the global transfer modality, and there we assumed that the size of the bundle,  $N$ , was very large. This enabled us to formulate the evolution of the system in terms of continuous differential equations. This type of equation, similar to those appearing in radioactivity, was first used by Coleman [8], and later in [11]. In [18] we supposed an ELS bundle formed by  $N$  fibres which breaks because of stress corrosion under the action of an external constant load  $F = N\sigma_0 = Y$ , with  $\sigma_0 = 1$ . The breaking rate of the fibres,  $\Gamma$ , is assumed to be of the power-law type ( $\Gamma = \sigma^\rho$ )  $f$  denotes the strain of the bundle and  $Y = 1$  represents the initial stiffness of the individual fibres. The original dynamic FBM was generalized by allowing one fibre to fail more than once, and thus we define the integer  $n$  as the maximum value of failures allowed per fibre. Besides, as mentioned before, the parameter  $a (< 1)$  represents the factor of reduction in the stiffness of the fibres when they fail. As up to  $n$  partial yielding events are permitted per fibre, at any one time the population of fibres will be sorted in  $n + 2$  lists. Thus  $N = N_0 + N_1 + \dots + N_n + N'$ , where  $N_i$  ( $i = 0, \dots, n$ ) denotes the number of elements that have failed  $i$  times.  $N'$  denotes the number of elements that have failed  $n + 1$  times and therefore are inactive (i.e., they no longer support any load anymore). At  $t = 0$ , the  $N$  elements of the bundle form the list 0,  $N_0 = N$ , and at  $t = T$ ,  $N' = N$ . The specification, at a given time  $t$ , of the value of  $N_i$ , for  $i = 0, 1, \dots, n$ , provides the state of the system. In our continuous formulation the  $N_i$  are real positive numbers lower than  $N$ .

As the external load  $F = N$  is supported by the present active fibres, we have  $N = f(N_0 + aN_1 + a^2N_2 + \dots + a^nN_n)$ , and hence

$$f = N / (N_0 + aN_1 + a^2N_2 + \dots + a^nN_n). \quad (1.1)$$

The time evolution equations are [18]:

$$\begin{aligned} \frac{dN_0}{dt} &= f^\rho(-N_0) \\ \frac{dN_1}{dt} &= f^\rho(N_0 - \kappa N_1) \\ \frac{dN_2}{dt} &= f^\rho\kappa(N_1 - \kappa N_2) \\ &\vdots \\ \frac{dN_n}{dt} &= f^\rho\kappa^{n-1}(N_{n-1} - \kappa N_n) \end{aligned} \quad (1.2)$$

where the ubiquitous constant factor  $\kappa$  represents  $\kappa = a^\rho$ . This is an autonomous differential system. Its solution must fulfill the initial condition

$$\begin{aligned} N_0(t = 0) &= N \\ N_j(t = 0) &= 0 \quad j \neq 0. \end{aligned} \quad (1.3)$$

An alternative way of introducing a time-dependent rheological response in FBM is that of Cruz-Hidalgo *et al* [19]. These authors incorporate a viscoelastic constitutive behaviour in

their model through the mapping of each fibre to a Kelvin–Voigt element. They express the time evolution of the strain in *each* fibre by way of a differential equation. In their model, fibres break irreversibly when they surpass a statistically distributed strain threshold, whereas in our model multiple failures (yields) of a fibre are allowed, the variable which is statistically distributed is the lifetime of the fibres, and there is no explicit threshold dynamics. This different formulation implies that we can formulate the evolution of the system in terms of coupled differential equations, while the authors in [19] have necessarily to use Monte Carlo simulations due to the absence of a global differential equation for the system.

In [18], equations (1.2) were solved by applying a numerical probabilistic method. The purpose of this paper is to present an exact numerical method that solves equations (1.2), fulfilling the initial conditions (1.3). This method is explained in section 2. In section 3 we present a discussion of the method and of the results. The reader will find a longer discussion of the physical results in [18]. This paper concentrates on the solution method.

## 2. Exact numerical method

To simplify the notation, we first normalize the variables

$$x_i = \frac{N_i}{N} \quad i = 0, 1, \dots, n. \quad (2.1)$$

In terms of the  $x_i$ , the differential system to be solved is

$$\begin{aligned} \dot{x}_0 &= -f^\rho x_0 & \dot{x}_j &= f^\rho \kappa^{j-1} (x_{j-1} - \kappa x_j) \\ x_0(0) &= 1 & x_j(0) &= 0 \quad j = 1, 2, \dots, n. \end{aligned} \quad (2.2)$$

A dot on a variable means derivation with respect to time, and  $f$  and  $\kappa$  are the same objects as in section 1:

$$1/f = \sum_{i=0}^n a^i x_i. \quad (2.3)$$

The system (2.2) admits a reduction of degrees of freedom by eliminating  $t$  from the last  $n$  equations and by integrating with respect to  $x_0$ :

$$\dot{x}_0 = -f^\rho x_0 \quad \frac{dx_j}{dx_0} = \frac{\kappa^{j-1} (\kappa x_j - x_{j-1})}{x_0}. \quad (2.4)$$

From equation (2.4) we obtain

$$x_i = \sum_{l=0}^i b_l^{(i)} x_0^{\kappa^l}, \quad i = 0, 1, \dots, n \quad (2.5)$$

with

$$\begin{aligned} b_0^{(0)} &= 1 & b_l^{(j)} &= \frac{b_l^{(j-1)} \kappa^{(j-1)}}{\kappa^j - \kappa^l} \\ b_j^{(j)} &= - \sum_{l=0}^{j-1} b_l^{(j)} & j &= 1, 2, \dots, n. \end{aligned} \quad (2.6)$$

In consequence,

$$f = \frac{1}{\sum_{i=0}^n a^i x_i} = \frac{1}{\sum_{i=0}^n \alpha_i x_0^{\kappa^i}} =: f_0(x_0) \quad \alpha_i = \sum_{l=i}^n a^l b_l^i. \quad (2.7)$$

Then, the first equation in (2.4) provides the relation  $x_0$  versus  $t$

$$t = \int_{x_0}^1 \frac{dx_0}{[f_0(x_0)]^\rho x_0} = \int_{x_0}^1 \frac{\left(\sum_{i=0}^n \alpha_i x_0^{\kappa^i}\right)^\rho}{x_0} dx_0 \tag{2.8}$$

which, in principle, solves the problem because it relates  $t$  to  $x_0$  and hence to any other  $x_j$ . However, the integral (2.8) is, in general, improper for  $x_0 \rightarrow 0$  because the integrand is  $O(x_0^{\rho\kappa^n-1})$  and therefore the numerical relation  $t$  versus  $x_0$  is problematic. Specifically:

- (a) If  $\rho\kappa^n - 1 \geq 0$  this integral is proper,
- (b) if  $\rho\kappa^n - 1 < 0$  the integral is improper.

Due to the fact that the convergence occurs iff  $\rho\kappa^n - 1 > -1$ , equation (2.8) is always convergent, because in our model of fracture  $\rho\kappa^n > 0$ .

Let  $\epsilon \in (0, 1)$ ; due to the fact that  $x_0$  decays from 1 to 0, there exists a time value  $t_0 > 0$  such that  $x_0(t_0) = \epsilon$ . If (2.8) is improper, we perform the following change of parameter:  $x_0 \equiv y_0 \rightarrow y_1$ , such that

$$\begin{aligned} \dot{x}_0 &= -f^\rho x_0 & \dot{y}_1 &= -\kappa f^\rho y_1 \\ \dot{x}_j &= f^\rho \kappa^{j-1} [x_{j-1} - \kappa x_j] & j &= 1, 2, \dots, n \end{aligned} \tag{2.9}$$

with  $x_0(t_0) = \epsilon, y_1(t_0) = 1$ , and  $t > t_0$ . From here

$$\frac{dx_0}{dy_1} = \frac{\kappa x_0}{y_1} \Rightarrow x_0 = c_1 y_1^{1/\kappa} \quad c_1 = (x_0(t_0)) = \epsilon. \tag{2.10}$$

Hence

$$x_j = \sum_{l=0}^j b_l^{(j)} \left(\epsilon y_1^{1/\kappa}\right)^{\kappa^l} = \sum_{l=0}^j \beta_l^{(j,1)} y_1^{\kappa^{l-1}} \tag{2.11}$$

$$f =: f_1(y_1) = \frac{1}{\sum_{i=0}^n \alpha_i \sum_{l=0}^i \beta_l^{(i,1)} y_1^{\kappa^{l-1}}} = \frac{1}{\sum_{i=0}^n \alpha_i^{(1)} y_1^{\kappa^{i-1}}} \tag{2.12}$$

with  $\beta_l^{(i,1)} = b_l^{(i)} \epsilon^{\kappa^l}, \alpha_i^{(1)} = \sum_{l=i}^n \alpha_l \beta_l^{(i,1)}$  ( $i = 0, 1, \dots, n$ ).

In these circumstances (2.11) and the equation

$$t - t_0 = \int_{y_1}^1 \frac{dy_1}{(f_1(y_1))^\rho y_1} = \int_{y_1}^1 \frac{\left(\sum_{i=0}^n \alpha_i^{(1)} y_1^{\kappa^{i-1}}\right)^\rho}{y_1} dy_1 \tag{2.13}$$

describe  $t, x_0, \dots, x_n$  in terms of the  $y_1$  parameter, for  $t \geq t_0$ .

As the integrand of (2.13) is  $O\left(y_1^{\rho\kappa^{n-1}-1}\right)$ , then

- (a) If  $\rho\kappa^{n-1} - 1 \geq 0$  then (2.13) is a proper integral,
- (b) if  $\rho\kappa^{n-1} - 1 < 0$  then (2.13) is an improper integral, but (2.13) is always convergent.

Now, as  $y_1$  decays to zero, there exists a time instant  $t_1 > t_0$  such that  $y_1(t_1) = \epsilon$ . And by considering the change of parameter  $y_1 \rightarrow y_2$  given by the conditions

$$\begin{aligned} \dot{x}_0 &= -f^\rho x_0 & \dot{y}_1 &= -\kappa f^\rho y_1 & \dot{y}_2 &= -\kappa^2 f^\rho y_2 \\ \dot{x}_j &= f^\rho \kappa^{j-1} [x_{j-1} - \kappa x_j] & j &= 1, 2, \dots, n \end{aligned} \tag{2.14}$$

with  $y_2(t_2) = \epsilon, y_2(t_1) = 1$ , and  $t > t_1$ , we have

$$\frac{dy_1}{dy_2} = \frac{\kappa y_1}{y_2} \Rightarrow y_1 = c_2 y_2^{1/\kappa} \quad c_2 = (y_1(t_1)) = \epsilon \tag{2.15}$$

**Table 1.** General terms in the procedure.

Time interval	Condition	Parameter
$[0, t_0]$		$y_0 = x_0$
$[t_0, t_1]$	$y_0(t_0) = \epsilon$	$y_1$ such that $\dot{y}_1 = -\kappa f^\rho y_1; y_1(t_0) = 1$
$[t_1, t_2]$	$y_1(t_1) = \epsilon$	$y_2$ such that $\dot{y}_2 = -\kappa^2 f^\rho y_2; y_2(t_1) = 1$
$\vdots$	$\vdots$	$\vdots$
$[t_{n-1}, t_n]$	$y_{n-1}(t_{n-1}) = \epsilon$	$y_n$ such that $\dot{y}_n = -\kappa^n f^\rho y_n; y_n(t_{n-1}) = 1$

and hence

$$x_j = \sum_{l=0}^j b_l^{(j,1)} (\epsilon y_2^{1/\kappa})^{\kappa^{l-1}} = \sum_{l=0}^j \beta_l^{(j,2)} y_2^{\kappa^{l-2}} \tag{2.16}$$

$$f =: f_2(y_2) = \frac{1}{\sum_{i=0}^n \alpha_i^{(2)} y_2^{\kappa^{i-2}}} \tag{2.17}$$

with identical meaning as before for  $\beta_l^{(j,2)}$  and  $\alpha_j^{(2)}$ . Then, (2.16) and

$$t - t_1 = \int_{y_2}^1 \frac{dy_2}{(f_2(y_2))^\rho y_2} = \int_{y_2}^1 \frac{\left(\sum_{i=0}^n \alpha_i^{(2)} y_2^{\kappa^{i-2}}\right)^\rho}{y_2} dy_2 \tag{2.18}$$

describe  $t, x_0, \dots, x_n$  in terms of  $y_2$ , for  $t \geq t_1$ . Besides, as the integrand of (2.18) is  $O(y_2^{\rho\kappa^{n-2}-1})$ , then

- (a) if  $\rho\kappa^{n-2} - 1 \geq 0$  then (2.18) is a proper integral,
- (b) if  $\rho\kappa^{n-2} - 1 < 0$  then (2.18) is an improper integral, but always convergent.

The process followed so far is generalized in the way expressed in table 1 where in the end

$$f =: f_n(y_n) = \frac{1}{\sum_{i=0}^n \alpha_i^{(n)} y_n^{\kappa^{i-n}}} \tag{2.19}$$

and therefore

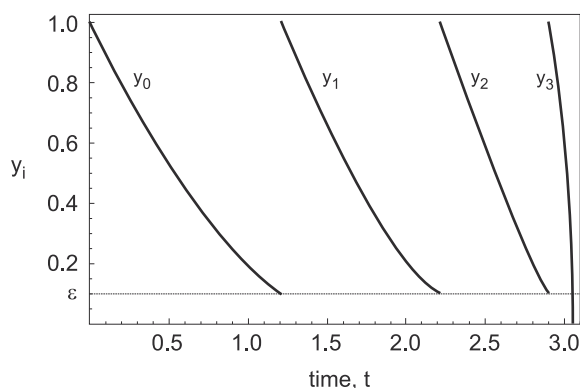
$$t - t_{n-1} = \int_{y_n}^1 \frac{dy_n}{(f_n(y_n))^\rho y_n} = \int_{y_n}^1 \frac{\left(\sum_{i=0}^n \alpha_i^{(n)} y_n^{\kappa^{i-n}}\right)^\rho}{y_n} dy_n \tag{2.20}$$

whose integrand is  $O(y_n^{\rho-1})$ ; that is, integral (2.20) is always proper.

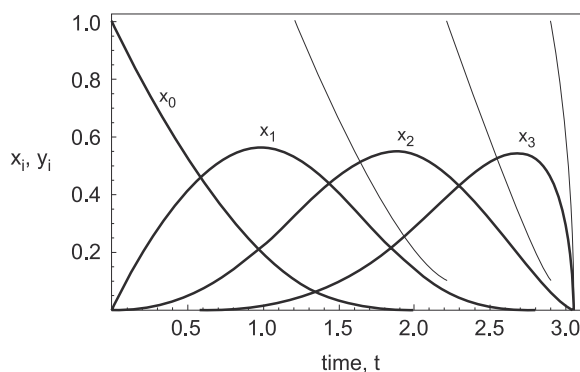
### 3. Results and conclusions

The simple formalism written in section 2 can be expressed, for example, in a brief program of MATHEMATICA and its results graphically appreciated. We omit here the program but it can be provided on request. By fixing the constants at the following values:  $n = 3, a = 0.6, \rho = 2$  and  $\epsilon = 0.1$ , in figure 1 the value of the working parameters  $y_i$  are represented versus time. Note that their range of definition is from 1 to  $\epsilon$ , except for  $y_3$  which ends at 0 for  $t_3 = T$ , i.e., the actual lifetime of the bundle.

In figure 2 we again show the evolution of the working parameters and also the evolution of the four lists  $x_i$  of elements in the problem.



**Figure 1.** Time evolution of the four integrating parameters  $y_0, y_1, y_2$  and  $y_3$  for a system with  $n = 3, a = 0.6$  and  $\rho = 2$ . Note that their range of definition is from 1 to  $\epsilon$ , except for  $y_3$ , which goes from 1 to 0.



**Figure 2.** Time evolution for the four integrating parameters and the four variables  $x_0, x_1, x_2$  and  $x_3$  for a system with the same parameters as for figure 1.

The strategy developed in section 2 can be summarized in a few sentences. First, let us observe figure 2 to appreciate the time evolution of the different lists: while  $x_0$  monotonously declines from 1 at  $t = 0$  to 0 at  $t = T$ , the lists  $x_j, j = 1, 2, 3$  start from 0 at  $t = 0$ , rise to a maximum and then monotonously decline to 0 at  $t = T$  (strictly speaking, all the lists vanish at the same time). The last list  $j = n$  is special in the sense that it is the only one that tends to 0 with an infinite slope when  $t$  tends to  $T$ .

The analytical resolution of equation (2.2) is impossible because of the nonlinearity introduced by the  $f^\rho$  factors. This source of complexity is partly overcome after having recognized the partial reduction of degrees of freedom expressed in (2.4). This partial reduction leads to the relation between  $x_j, j = 1, 2, \dots, n$  and  $x_0$ , hence from (2.8) one has solved in principle the time evolution of  $x_0$ , and of the rest of  $x_j$ . But, in (2.8) one also recognizes that this integral is improper. This is the *real problem* we face for the numerical inversion  $t \leftrightarrow x_0$  in the region where  $x_0$  is very small. In intuitive terms, this is shown in figure 2 because beyond a certain time,  $x_0$  is no longer significant and its relation with  $t$  becomes ‘delicate’. Therefore, we have used  $x_0 = y_0$  as a good integration parameter only up to  $t = t_0$ . Beyond this point we successively introduced other ‘artificial parameters’  $y_1, y_2, \dots, y_n$  which in the corresponding time interval play the role performed by  $x_0$  from 0 to  $t_0$ . Using these

parameters, we are able to robustly relate all the variables  $x_i$  to  $t$  in the whole interval from 0 to  $T$ .

At the end of the process, the last integral is always proper, which allows a robust numerical inversion in the vicinity of  $t = T$ . Intuitively, this is clear in figure 2 where we appreciate the abrupt fall-off of  $x_3$ .

In the comments written in section 2 after equations (2.8), (2.13), (2.18) and (2.20) regarding the nature of those integrands, we noted that in general they behave as  $O(y_i^{\rho\kappa^{n-i}-1})$ . This implies that the condition

$$\rho\kappa^{n-i} - 1 \geq 0 \quad (3.1)$$

tells us the value of  $i = i_c$ ,

$$i_c \geq n - \frac{\ln \rho}{|\ln \kappa|} \quad (3.2)$$

such that, for  $i \geq i_c$ , the respective integral is proper and there is no need to introduce more artificial integrating parameters.

The reader should note that the  $\epsilon$  introduced in the method is not a limiting factor of precision, but merely sets the temporal ranges of the various integrating parameters  $y_i$ . In our procedure, the only source of inaccuracy is the precision of MATHEMATICA, used for the numerical inversion of the integrals.

As a final conclusion we would say that the exact numerical method presented in this paper to solve this fibre-bundle problem does not predict any new qualitative result with respect to what was obtained using the approximate method of [18]. Therefore, no new physical conclusions can be drawn from here.

The use of this exact strategy in other scientific problems that are cast as an autonomous differential system will be considered in the next future. In this respect, clear candidates are some ecological problems and models of infection spreading [20, 21].

## Acknowledgment

This work was supported in part by the Spanish DGICYT Project PB98-1594.

## References

- [1] Herrman H J and Roux S (eds) 1990 *Statistical Models for the Fracture of Disordered Media* (Amsterdam: North Holland) and references therein
- [2] Chakrabarti B K and Benguigui L G 1997 *Statistical Physics of Fracture and Breakdown in Disordered Systems* (Oxford: Clarendon Press) and references therein
- [3] Garcimartin A, Guarino A, Bellon L and Ciliberto S 1997 *Phys. Rev. Lett.* **79** 3202
- [4] Maes C, van Moffaert A, Frederix H and Strauven H 1998 *Phys. Rev. B* **57** 4987
- [5] Petri A, Paparo G, Vespignani A, Alippi A and Constantini M 1994 *Phys. Rev. Lett.* **73** 3423
- [6] Zapperi S, Ray P, Stanley H E and Vespignani A 1997 *Phys. Rev. Lett.* **78** 1408
- [7] Moreno Y, Gomez J B and Pacheco A F 2000 *Phys. Rev. Lett.* **85** 2865
- [8] Coleman B D 1957 *J. Appl. Phys.* **28** 1058  
Coleman B D 1957 *J. Appl. Phys.* **28** 1065
- [9] Phoenix S L and Tierney L 1983 *Eng. Fract. Mech.* **18** 193
- [10] Newman W I, Gabrielov A M, Durand T A, Phoenix S L and Turcotte D L 1994 *Physica D* **77** 200
- [11] Newman W I, Turcotte D L and Gabrielov A M 1995 *Phys. Rev. E* **52** 4827
- [12] Vázquez-Prada M, Gómez J B, Moreno Y and Pacheco A F 1999 *Phys. Rev. E* **60** 2581
- [13] Zapperi S, Vespignani A and Stanley H E 1997 *Nature* **388** 658
- [14] Kun F, Zapperi S and Herrmann H J 2000 *Eur. Phys. J. B* **17** 269



- 
- [15] Naaman A E and Reinhardt H W 1995 *High Performance Fibre Reinforced Cement Composites* (London: Spon)
  - [16] Evans A G, Domergue J M and Vagaggini E 1994 *J. Am. Ceram. Soc.* **77** 1425
  - [17] Kanada T and Li V C 1999 *J. Eng. Mech.* **125** 290
  - [18] Moral L, Moreno Y, Gómez J B and Pacheco A F 2001 *Phys. Rev. E* **63**
  - [19] Cruz-Hidalgo R, Kun F and Herrmann H 2001 *Preprint cond-mat/0103232*
  - [20] Rama Mohana Rao M 1981 *Ordinary Differential Equations: Theory and Applications* (London: Arnold)
  - [21] Anderson B M and May R M 1992 *Infection Diseases in Humans* (Oxford: Oxford University Press)